MANN CREEK RESERVOIR 1992 SEDIMENTATION SURVEY

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U.S. Department of the Interior Bureau of Reclamation

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1992 SEDIMENTATION SURVEY

by

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July 1992

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INTRODUCTION

Mann Creek Dam and Reservoir, major features of the Mann Creek Project, are located on Mann Creek in the Weiser River Basin. The dam, located in Washington County, Idaho, is about 13 miles northeast of Weiser, Idaho. The dam was designed and constructed as Spangler Dam, but its name was officially changed to Mann Creek Dam prior to completion (fig. 1).

In 1938, Reclamation (Bureau of Reclamation), investigated the Spangler Reservoir site on Mann Creek for developing an irrigation water supply. The project was approved for construction in July 1941 under the terms of the Water Conservation and Utilization Act. The landowners of the Mann Creek area failed to approve the proposed repayment contract and the project was not constructed. A new study was prepared on an alternative Spangler Reservoir site in 1958, followed by authorization and development of a definite plan. The Mann Creek Project was authorized for construction under the provisions of Public Law 87-589, approved August 16, 1962.

Construction of Mann Creek Dam and Reservoir began in 1965, and was completed in 1967. Initial water storage began on March 27, 1967. The dam was constructed as a zoned earth and rockfill structure. The reservoir was designed to provide water for supplemental irrigation in the Mann Creek and Monroe Creek areas. Actual operation showed flood control, recreation, and fish and wildlife benefits. Mann Creek Dam and Reservoir and all other project facilities are operated by the Mann Creek Irrigation District.

At dam crest elevation 2903.0, Mann Creek Dam (fig. 2) has:

- a structural height^{*} of 148 feet
- a hydraulic height of 132 feet
- a top crest width of 30 feet
- a crest length of 1,176 feet

The spillway, located along the right abutment, consists of a morning-glory-type inlet structure with an uncontrolled ogee crest at elevation 2889.0, a 24-inch air inlet pipe, and a circular 11-foot cut-and-cover conduit discharging into a stilling basin located along the right abutment. The spillway design flow is 3,840 cubic feet per second at maximum water surface elevation 2897.1.

The outlet works, located along the left abutment, is controlled by two 2.25-square-foot high pressure gates located in a control house and one 2.75-foot high-pressure gate located in the gate chamber for emergency. The capacity of the outlet works is 300 cubic feet per second at reservoir elevation 2889.0.

The 1992 reservoir survey measured a total storage capacity of 12,536 acre-feet and a surface area of 283 acres at reservoir spillway crest elevation 2889.0.

^{*} The definition of terms such as "structural height," "hydraulic height," etc., may be found in manuals such as Reclamation's *Design of Small Dams* and *Guide for Preparation of Standing Operating Procedures for Dams and Reservoirs*, or ASCE's *Nomenclature for Hydraulics*.

SUMMARY AND CONCLUSIONS

This report presents the 1992 results of the first extensive sedimentation survey of Mann Creek Reservoir by Reclamation since construction of Mann Creek Dam. The primary objectives of the survey were to:

- gather data needed for developing new reservoir topography
- compute area-capacity relationships
- estimate storage depletion caused by sediment deposition since closure of Mann Creek Dam.

Standard land surveying methods were used to establish horizontal and vertical control points for the aerial and hydrographic surveys. A horizontal grid system was established for both surveys using monumented control points located in the reservoir area. The bathymetric survey was run using sonic depth recording equipment interfaced with an automated survey system consisting of a line-of-sight microwave positioning unit capable of determining sounding locations within the reservoir. The system continuously recorded reservoir depth and horizontal coordinates as the survey boat was steered across close-spaced gridlines covering the reservoir area. The positioning system provided information to allow the boat operator to maintain course along these gridlines. Water surface elevations measured by the land surveyors at the time of data collection were used to convert the sonic depth measurements to true lake bottom elevations.

The 1992 surface areas at predetermined 5-foot contour intervals were generated by a computer graphics program that produced a new contour map of the reservoir (fig. 3). The revised area and capacity tables were produced by a computer program that uses measured contour surface areas and a curve-fitting technique to compute area and capacity at prescribed elevation increments.

Table 1 contains a summary of reservoir watershed characteristics and sediment data for the 1992 survey. The 1992 survey determined that the reservoir has a storage capacity of 12,536 acre-feet and a surface area of 283 acres at spillway crest elevation 2889.0. Since closure in 1967, the reservoir has accumulated a volume of 555 acre-feet of sediment below spillway crest elevation 2889. This volume represents a 4.44-percent loss in total capacity and an average annual loss of 22.0 acre-feet. These figures indicate a small amount of sediment accumulated in the reservoir since the original survey, but a high percentage of volume loss for this small time period because of the small storage capacity of Mann Creek Reservoir. For sediment calculation purposes the difference between the original and 1992 capacity was used, but a question exists as to the accuracy of the original area-capacity. A resurvey of Mann Creek Reservoir should be considered in the future if major sediment inflow events occur or if a more accurate rate of sediment accumulation is needed.

DESCRIPTION OF WATERSHED

Mann Creek, which drains into Mann Creek Reservoir, originates in the Payette National Forest on the southern slopes of the Hitt Mountains. The watershed above the dam has a drainage area of about 56 square miles. Elevations in the watershed range from 2822.0 at the outlet works to about 7400 feet along the northwestern divide. The runoff of Mann Creek originates almost entirely from melting snow. The topography, climate, and cover on the watershed is conducive to high spring runoff and low flow during the summer and winter months. The creek flows generally south-southeast in a rather narrow canyon.

The basin is characterized by steeply sloping hills and canyon walls covered with sparse grasses and sagebrush in the lower elevations of the watershed. The upper elevations of the watershed tend to be mountainous terrain with moderate to steep slopes covered with a medium dense growth of pine trees and grasses. The soil throughout the watershed is a silty clay loam.

RESERVOIR OPERATIONS

The reservoir is a multiuse facility having (following values are from June 1992 area-capacity tables):

- 2,419 acre-feet of exclusive flood control storage between elevations 2889.0 and 2897.1
- 10,917 acre-feet of active conservation storage between elevations 2825.0 and 2889.0
- 224 acre-feet of inactive storage between elevations 2822.0 and 2825.0
- 1,395 acre-feet of dead storage between elevations 2782.7 and 2822.0

Records for Mann Creek Reservoir show an average unregulated inflow of 30,535 acre-feet per year. The estimated mean annual runoff from the basin is 10.2 inches. Mann Creek Reservoir operation ranged from a minimum elevation of 2825.0 in September 1988 and 1992 to a maximum elevation of 2890.8 in April 1990. The inflow and end-of-month stage records in table 1 show the extreme annual fluctuation of the reservoir.

SURVEY METHOD AND EQUIPMENT

The Mann Creek Reservoir survey was completed using the contour method as outlined by Blanton (1982). The procedure involved collecting adequate coordinate data for developing a reliable contour map by photogrammetric and bathymetric survey methods. Standard land surveying methods were used by Columbia Basin Project Office personnel to establish horizontal and vertical control points for both survey methods. A horizontal grid system was established for both surveys using monumented points, with state plane coordinates, located in the reservoir area. The above water data were collected by aerial photography prior to the bathymetric survey. The field survey work for the bathymetric survey involved establishing a triangulation network around the reservoir to provide horizontal and vertical control for all required grid lines and shore stations. No previously established range lines existed on the lake, and it was decided not to establish permanent range lines during this survey. Because of the size and shape of the reservoir, any future survey would also employ the contour method; therefore, permanent range line end markers were not necessary.

The hydrographic survey was run on June 3, 1992, with the reservoir at water surface elevation 2866.9. The bathymetric survey was run using sonic depth recording equipment interfaced with an automated survey system consisting of a line-of-sight microwave positioning unit capable of determining sounding locations within the reservoir. This positioning system transmitted line-of-sight microwave signals to fixed shore stations and converted the reply time to range distances, which were used by the system data logger to compute the coordinate position of the sounding boat. The survey system continuously recorded reservoir depth and horizontal coordinates as the survey boat moved across closespaced gridlines covering the reservoir area. To produce adequate data for developing contours of Mann Creek Reservoir, grid spacing of 150 feet was selected. The system gave directions to the boat operator to assist in maintaining course along the close-spaced gridlines. During each run, the depth and position data were recorded on a floppy disk for subsequent processing by Denver Office personnel. A graph plotter was used in the field to track the boat and ensure adequate coverage during the collection process. Water surface elevations surveyed at the time of collection were used to convert the sonic depth measurements to true lake bottom elevations.

RESERVOIR AREA AND CAPACITY

Original Capacity

The original total capacity of Mann Creek Reservoir was reported as 12,950 acre-feet at the spillway crest elevation of 2889.0. For determining change in reservoir storage, the original storage-elevation relationship was recomputed using 5-foot surface area values from the October 1967 area-capacity tables for elevations 2825.0 through 2897.1, and September 1964 preliminary area values for elevations 2760.0 through 2820.0. Some question exists as to the accuracy of the original topography and resulting reservoir surface areas. A note on Reclamation drawing 354-D-45 indicates that the map topography does not agree in all cases with the ground surface elevations surveyed at the reservoir borrow areas.

Results of the original area and capacity computations are listed in table 1 and in columns (2) and (3) of table 2. The original measured surface area values at elevations 2865.0, 2870.0, 2875.0, 2890.0, and 2897.1 were found to be slightly less than the 1992 survey values at the same elevation. This difference resulted in the 1992 survey showing a slight gain of volume in the upper reservoir area compared to the original survey. As illustrated in table 2, the survey also showed the largest measured sediment volume, column (6), at elevation 2860.0. Spillway crest elevation 2889.0 was used when computing all sediment accumulation values because little sign of bank erosion was observed and these small gains in surface area were assumed to be the result of the different survey methods.

Development of 1992 Contour Areas

The 1992 contour surface areas for Mann Creek Reservoir were developed by generating a contour map from the collected aerial and underwater coordinate data. Five-foot contour intervals of the lake area were created by a computer graphics software program SURFACE II (Kansas Geological Survey, 1978). A modification of this program by the Denver Office calculated surface areas of the closed contours of the generated map. The final reservoir map shown on figure 3 was prepared by the Denver Office Computer Drafting Unit of the Drafting Section. The map has a scale of one inch equals 300 feet and a contour interval of five feet.

1992 Revised Storage Capacity

The storage-elevation relationships based on the aerial and underwater survey data were developed using the area-capacity computer program ACAP85 (Reclamation, 1985). Surface areas at 5-foot contour intervals computed from the aerial and underwater survey data were used as the control parameters for computing reservoir capacity. The program computes an

area at elevation increments of 0.01 to 1.0 foot by linear interpolation between the 5-foot contour intervals. The program begins by testing the initial capacity equation over successive intervals to ensure that the equation fits within an allowable error limit, which was set at 0.000001 for Mann Creek Reservoir. This capacity equation is then used over the full range of intervals fitting within this allowable error limit. For the first interval at which the initial allowable error limit is exceeded, a new capacity equation (integrated from the basic area curve over that interval) tests the fit until it also exceeds the error limit. Thus, the capacity curve is defined by a series of curves, each fitting a certain region of data. Final area equations are derived by differentiating the capacity equations, which are of second order polynomial form:

$$y = a + a_2 x + a_3 x^2$$

where:

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y = capacity, x = elevation above a reference base, a = intercept, and a_2 and $a_3 =$ coefficients

Results of the 1992 Mann Creek Reservoir area and capacity computations are listed in table 1 and columns (4) and (5) of table 2. Listed in columns (2) and (3) of table 2 are the original surface areas and recomputed capacity values. A separate set of 1992 area and capacity tables has been published for the 0.01-, 0.1-, and 1-foot elevation increments (Reclamation, 1992). A description of the computations and coefficients output from the ACAP85 program is included with these tables. Both the original and 1992 area-capacity curves are plotted on figure 4. As of June 1992, at reservoir spillway crest elevation 2889.0, the surface area was 283 acres, with a total capacity of 12,536 acre-feet and an active capacity of 10,917 acre-feet.

SEDIMENT ANALYSES

Sediments have accumulated in Mann Creek Reservoir to a total volume of 555 acre-feet since dam closure in March 1967. Of the total deposited sediment, 209 acre-feet was deposited in the active pool and 376 acre-feet in the inactive pool storage areas. The average annual rate of sediment deposition between closure and June 1992 (25.2 years) was 22.0 acre-feet per year, or 0.168 acre-foot per square mile from the sediment contributing drainage area. The storage loss in terms of percent of original storage capacity was 4.44 percent. The 555 acre-feet of sediment is a small amount to have accumulated in the reservoir since the original survey, but a high percentage of volume loss for the small capacity of Mann Creek Reservoir. Table 1 and 2 contain the Mann Creek Reservoir sediment accumulation and water storage data based on the 1992 resurvey.

A 1987 study to estimate sediment accumulations (Reclamation, 1987c) was initiated at Mann Creek Reservoir to address concerns that timber harvest, depleted range cover, and channel alterations cause excessive erosion in the watershed. Depth-integrated suspended sediment samples were collected intermittently in Mann Creek above the reservoir in 1984 and 1985, and mean daily discharges were calculated from reservoir releases and daily change in contents. A flow frequency distribution was determined from average daily inflows during the 1968-86 period of record. The flow duration data were combined with the sediment rating curve to determine average annual suspended sediment inflow. Based on the available data, the study estimated a 100-year sediment accumulation of 217 acre-feet, which was less than 2 percent of the total storage capacity.

Several factors must be considered when using either the 1987 or 1992 study results. The 1987 study only had a few samples and an estimated mean daily discharge on which calculations could be based. This method does not account for any major sediment inflow event that may have occurred. The 1992 study sediment calculations were based on the difference between the original and 1992 measured reservoir capacities. This method would account for all sediment accumulation during the 25.2 years of reservoir operation, but the calculations are only as accurate as the reservoir topography maps. The original reservoir and vicinity map, Drawing No. 354-D-45, notes that ground surface profile elevations surveyed at the auger hole locations do not agree in all cases with the map topography. This discrepancy brings into question the accuracy of the original areas and capacities which were used as the base for measuring the accumulated sediment in 1992. For sediment calculation purposes, the difference between the original and 1992 capacity was used, but as noted, a question exists as to the accuracy of the original area-capacity. A resurvey of Mann Creek Reservoir should be considered in the future if major sediment inflow events occur, or if the average annual rate of sediment accumulation requires clarification.

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Kansas Geological Survey, SURFACE II GRAPHICS SYSTEM, Lawrence, Kansas, 1978.

RESERVOIR SEDIMENT DATA SUMMARY

Mann Creek Reservoir NAME OF RESERVOIR

				F.	NAME	OF RESERV	DIR			1		
										DATA SHEE	T NO.	
D	1. OWNER Bureau	of Reclamat	ion		2. STREAM Mann Creek				3. STATE Idaho			
A	4. SEC. 11 TWP.	12N RANG	JE 5W		5. NEA	REST P.O.	Veiser	2	6. C	6. COUNTY Washington		
м	7. LAT 44° 23' 3	1" LONG 1	L6° 53'	38"	8. TOF	OF DAM E	LEVATI	ION 2903.0	9. S	PILLWAY CRES	T 2889.0	
R E	10. STORAGE ALLOCATION	12. ORIG SURFACE	INAL AREA, Ac	13. CAPA	ORIGINAL CITY, AF	14. GRO ACRE- 1	4. GROSS STORAGE 15. I CRE- FEET STOR		lte Se			
E	a. FLOOD CONTROL 2897.1			313			2	2,410	15,	,360	- DEUAR	
R	b. MULTIPLE USE	288	9.0		2	83	11	,100	12	,950	3/27/	67
ŏ	c. POWER										7	
I	d. WATER SUPPLY										16. D/	TE
K	e. IRRIGATION							•				ION
	f. CONSERVATION										BEGAN	
	g. INACTIVE	282	5.0			84	1	,850	1,	,850	3/27	67
	17. LENGTH OF RES	SERVOIR		1	6	MILES	AVG.	WIDTH OF RES	ERVOIR	0	.28 MI	LES
B	18. TOTAL DRAINAG	GE AREA		56	5 SQUA	RE MILES	22.	MEAN ANNUAL P	RECIPITA	TION 11	.5 ¹ IN	CHES
ŝ	19. NET SEDIMENT	CONTRIBUTI	NG ARE	A 56	5 SQUA	RE MILES	23.	MEAN ANNUAL R	UNOFF	10	. 2* IN	CHES
IN	20. LENGTH	MILES	AV.	WIDTH	i Mi	LES	24.	MEAN ANNUAL R	UNOFF	30,5	353 ACRE-	FEET
	21. MAX. ELEVATIO	DN 7400	MIN	. ELEV	ATION 28	25.0	25.	ANNUAL TEMP.	MEAN 50	F RANGE -2	5 F to 10	5"F'
S U R	26. DATE OF SURVEY	27. 2 PER. A YRS. Y	8. CCL. RS.	29. T SURVE	YPE OF Y	30. NO. C RANGES OF INTERVAL)F	31. SURFACE AREA, AC.	32. ACRI	CAPACITY E-FEET	33. C/I RATIO	AF/AF
Ĕ	3/27/67			Cont	our(R)			2834		13,091		0.43
Y												
D A	6/3/92	25.2 2	5.2	Cont	our(D)	5-1t		283.0		12,536		0.41
T A	26. DATE OF SURVEY	34. PERIC ANNUAL PRECIP		35. P	ERIOD WAT	ER INFLOW,	ACRE	FEET	WATI	ER INFLOW TO	DATE, A	?
				a. ME	AN ANN.	b. MAX. A	NN.	c. TOTAL	a. 1	TEAN ANN.	b. TOTA	T
• • •	6/3/92	1	1.5	3	0,535	68,60	0	769,480°		30,535	769,	480
b ,	26. DATE OF SURVEY	37. PERIC	D CAPA	CITY L	OSS, ACRE	-FEET		38. TOTAL SP	DIMENT	DEPOSITS TO	DATE, AF	
		a. TOTAL		b. AV	. ANN.	c. /MI.1-	YR.	a. TOTAL	b. 4	AV. ANNUAL	c. /MI.	*-YR.
	6/3/92	55:	56		22.0		0.39	.555		22.0		0.39
	26. DATE OF SURVEY	. DATE OF 39. AV. DRY 40. RVEY WT. (#/FT ³)		40. S	ED. DEP.	TONS/MI.2-Y	R.	41. STORAGE LO		OSS, PCT.		IMENT PPM
				a. PE	RIOD	b. TOTAL DATE	TO	a. AV. ANNUAL	b. DATI	FOTAL TO E	a. PER.	b. TOT.
	6/3/92							0.168'		4.447		
26.	43. DEPTH DE	SIGNATION I	RANGE I	N FEET	r below se	PILLWAY CRE	ST ELI	EVATION				-

	DATE														
	of Survey		129.	0- 11	9.0-	109.0-	99.0-	89.0-	79.0-	69.0-	59.0-	49.0	- 39	0.0-	29.0-
			119.	0 10	9.0	99.0	89.0	79.0	69.0	59.0	49.0	39.0	29	<u>, 0 </u>	crest
			PERCENT OF TOTAL SEDIMENT LOCATED WITHIN DEPTH DESIGNATION												
	6/3/92		2	.7	9.7	17.0	7.8	10.9	13.0) 12.8	11.1	. 11.	4	3.6	0.0
	26. DATE	44. RI	ACH DES.	IGNATIO	N PERCI	ENT OF TO	TAL ORIG	INAL LENG	TH OF RES	ERVOIR					
		0-10	10-	20-	30-	40-	50-	60-	70- 80	- 90-	100-	105-	110-	115-	120-
	SURVEY		20	30	40	50	60	70	80 9	0 100	105	110	115	120	125
					PE	RCENT OF	TOTAL SI	EDIMENT L	OCATED WI	THIN REACH	DESIGNAT	TION			

Table 1. - Reservoir sediment data summary (page 1 of 2).

	Drerbunit np	FDATION				Contraction of the local data					
WATER VEAR	MAX FIFY MIN FLF				FILW	WATER YEAR		MAX ELEV.		MIN ELEV	I INFLOW AF
1967	2000 1	2840.8	<u> </u>	10 200		1069		2889 2		2848 9	15 400
1969	2889 4	2849 8		32 800		1970	1000	2889.3		2852 5	34 600
1971	2889.8	2851.8		51,800		1972		2889.5		2835.9	32,000
1973	2889.6	2837.5		16,300		1974		2.8	89.6	2837.3	47.200
1975	2889.9	2843.3		38,700		1976		28	89.0	2847.5	24,200
1977	2854.8	2826.3		2.800		1978		28	90.1	2828.0	42,400
1979	2889.7	2838.9		20,200		1980		28	89.9	2838.0	28,900
1981	2889.7	2841.5		20,300		1982		28	89.9	2843.3	53,700
1983	2888.6	2859.5		68,600		1984		28	89.3	2851.6	50,000
1985	2888.3	2846.4		24,200		1986		28	89.7	2840.8	36,000
1987	2889.8	2825.6		13,900		1988		28	79.7	2825.0	10,940
1989	2889.3	2825.6		43,020		1990		28	8.008	2839.1	17,450
1991	2889.6	2829.4		14,650		1992		28	80.8	2825.0	10,220*
46. ELEVATIO	ON - AREA - C	APACITY DATA	FOR ORIG	INAL CAP	ACITY .						
ELEV.	AREA	CAP.	ELEV.	A	AREA		CAP.		ELEV.	AREA	CAP.
2760	0	0	2805		45.4		676		2855	160	5,590
2765	1.5	4	2810		56.0	- 1	930		2860	178	6,435
2770	3.0	15	2815		66.1		1,235		2865	195	7,368
2775	5.3	36	2820		77.0		1,593		2870	211	8,383
2780	8.0	69	2825		84		1,995		2875	230	9,485
2702.7	(11)	94	2830		9/		2,448		2880	251	10,688
2/85	13.0	121	2835		108	- 1	2,960		2885	269	11,988
2790	19.0	201	2840		118	- 1	3,525		2889	(283)	13,091
2/95	26.8	316	2845		130		4,145		2890	286	13,3/5
AE FLEVATI	DN - APEA - C	470	2000 1002	TOTAL C	ADACTTY	4,830		2097.1		313	15,302
FLEV	AREA	CAP	FLEV	IUIAL G	REA		CAP	— 1	FLEV	ARFA	
		· · · ·								- Inclui	7 000
2782.7	0	0	2825		77.6		1,619		2870	214.1	1.043
2782.7 2785	0 1.2	0 1	2825 2830		77.6 90.1		1,619 2,038		2870 2875	214.1 230.2	8,934
2782.7 2785 2790	0 1.2 13.6	0 1 38	2825 2830 2835		77.6 90.1 101.4		1,619 2,038 2,517		2870 2875 2880	214.1 230.2 250.4	8,934 10,135
2782.7 2785 2790 2795	0 1.2 13.6 23.2	0 1 38 130	2825 2830 2835 2840		77.6 90.1 101.4 113.0	·	1,619 2,038 2,517 3,053		2870 2875 2880 2885	214.1 230.2 250.4 268.6	8,934 10,135 11,433
2782.7 2785 2790 2795 2800	0 1.2 13.6 23.2 31.1	0 1 38 130 266	2825 2830 2835 2840 2845		77.6 90.1 101.4 113.0 123.6		1,619 2,038 2,517 3,053 3,644		2870 2875 2880 2885 2889	214.1 230.2 250.4 268.6 (283)	8,934 10,135 11,433 12,536
2782.7 2785 2790 2795 2800 2805	0 1.2 13.6 23.2 31.1 39.4	0 1 38 130 266 442	2825 2830 2835 2840 2845 2850		77.6 90.1 101.4 113.0 123.6 136.6		1,619 2,038 2,517 3,053 3,644 4,295		2870 2875 2880 2885 2889 2890	214.1 230.2 250.4 268.6 (283) 286.7	8,934 10,135 11,433 12,536 12,821
2782.7 2785 2790 2795 2800 2805 2810	0 1.2 13.6 23.2 31.1 39.4 48.8	0 1 38 130 266 442 663	2825 2830 2835 2840 2845 2850 - 2855		77.6 90.1 101.4 113.0 123.6 136.6 154.4		1,619 2,038 2,517 3,053 3,644 4,295 5,022		2870 2875 2880 2885 2889 2890 2897.1	214.1 230.2 250.4 268.6 (283) 286.7 314.0	8,934 10,135 11,433 12,536 12,821 14,955
2782.7 2785 2790 2795 2800 2805 2810 2815	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8	0 1 38 130 266 442 663 934	2825 2830 2835 2840 2845 2850 2855 2850 2855 2860		77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7		1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2	0 1 38 130 266 442 663 934 1,254	2825 2830 2835 2840 2845 2850 2855 2860 2865		77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2		1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A Project D	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro.	2825 2830 2835 2840 2845 2850 2855 2860 2865 2860 2865	966 - 80,	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR.		1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A ¹ Project D ² Calculate	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff	2825 2830 2835 2840 2845 2850 2855 2860 2865 2860 2865 ject, 19 value o	966 - 80, of 30,535	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite	em 24	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A ¹ Project D ² Calculate ³ Unregulat	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE ata Book of M d using mean ed monthly in	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records :	2825 2830 2835 2840 2845 2855 2860 2865 2865 ject, 19 value o for rese	966 - 80, of 30,535 ervoir op	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite peration	em 24 peri	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	7,823 8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A Project D ² Calculate ³ Unregulat ⁴ Surface a	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean ed monthly in rea at reserv	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records : oir elevation	2825 2830 2835 2840 2845 2850 2855 2860 2865 ject, 19 value o for rese 2889.0.	966 - 80, of 30,535 prvoir op	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite	em 24 peri	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790		2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	8,934 10,135 11,433 12,536 12,821 14,955 16,876
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS / Project D ² Calculate ³ Unregulat ⁴ Surface a ⁵ Capacity question as	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean ed monthly in rea at reserv at elevation s to the accus	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records : oir elevation 2889.0. Compracy of the or	2825 2830 2835 2840 2845 2850 2855 2860 2865 ject, 19 value o for rese 2889.0.	966 - 80, of 30,535 ervoir op Reclamat surface	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite peration	em 24 peri CAP 1	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790 4).	ising	2870 2875 2880 2885 2899 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8	Some
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A ¹ Project D ² Calculate ³ Unregulat ⁴ Surface a ⁵ Capacity question as ⁶ Total cap crest eld EL. 2870	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE ata Book of M d using mean ed monthly in rea at reserv at reserv at elevation s to the accur acity loss ca evation 2889. , and E1. 2889. capacity loss	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records : oir elevation 2889.0. Computed flow records : oir elevation 1000 cm flow records : 0 cm	2825 2830 2835 2840 2845 2850 2855 2860 2865 ject, 19 value o for rese 2889.0. ited by iginal probably ordeal a	Reclamat surface of recompu ured slig y due the t elevat:	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite beration Cion's AC areas. ted capa ghtly gr e differ ion 2860	em 24 peri CAP y acity ceate cence	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790 4). iod. y (see reprint of the sum	ising mark rigin	2870 2875 2880 2885 2889 2890 2897.1 2903 original s al areas (ethods and	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8 336.8 992 capacity at <22) at El. 28 (/or some bank	Some spillway 65, erosion.
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A Project D ² Calculate ³ Unregulat ⁴ Surface a ⁵ Capacity question as ⁶ Total cap crest ele EL. 2870 Maximum of Average as at EL. 24	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean ed monthly in rea at reserv at elevation s to the accus acity loss ca evation 2889. , and EL. 289 capacity loss nnual and tot 889.0 computed	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records : oir elevation 2889.0. Comp racy of the or lculated by c. The 1992 are 7.1 which was of 585 AF records al sediment do	2825 2830 2835 2840 2845 2855 2860 2855 2860 2865 ject, 19 value o for rese 2889.0. ited by iginal is probabl corded a eposits g origin	Reclamat surface of recompu- ured slig y due that t elevat: of 22.0 nal surface	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite beration Cion's AC areas. ted capa ghtly gr e differ ion 2860 AF and 5 ace area	em 24 peri CAP y acity cence cence cence s555 A a dat	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790 4). iod. y (see re er then o es in sur to this AF respecta	using mark rigin vey m	2870 2875 2880 2885 2889 2890 2897.1 2903	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8 336.8 992 capacity at <27) at E1. 28 (/or some bank by 13,091 AF.	Some Some Some Some Some Some Some Some
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A ¹ Project D ² Calculate ³ Unregulat ⁴ Surface a ⁵ Capacity question as ⁶ Total cap crest eld E1. 2870 Maximum 7 Average a at E1. 24 ⁹ Calculate	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean ed monthly in rea at reserv at elevation s to the accur acity loss ca evation 2889. , and E1. 289 capacity loss nnual and tot 889.0 computed d inflow for	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro. annual runoff flow records : oir elevation 2889.0. Comp racy of the oil 1culated by cc The 1992 are 7.1 which was of 585 AF records al sediment de d by ACAP usin Oct. 1991 three	2825 2830 2835 2840 2845 2850 2855 2860 2865 ject, 19 value o for rese 2889.0. ited by iginal corded as posits or origin	Reclamat surface a recompu ured slig y due that t elevat: of 22.0 nal surface y 1992.	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite beration Careas. ated capa ghtly gr e differ ion 2860 AF and 5 ace area	em 24 peri carity reate rence due 555 A a dat	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790 4). iod. 4). iod. y (see respectively of the second s	asing mark brigin vey m	2870 2875 2880 2885 2889 2890 2897.1 2903 #5) and 19 al areas (ethods and y divided	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8 336.8 992 capacity at <27) at E1. 28 //or some bank by 13,091 AF.	Some spillway 65, erosion. Capacity
2782.7 2785 2790 2795 2800 2805 2810 2815 2820 47. REMARKS A Project D ² Calculate ³ Unregulat ⁴ Surface a ⁵ Capacity question as ⁶ Total cap crest eld EL. 2870 Maximum d ⁷ Average a at EL. 24 ⁹ Calculate ⁹ Original from 10/6 original su	0 1.2 13.6 23.2 31.1 39.4 48.8 59.8 68.2 AND REFERENCE: ata Book of M d using mean ed monthly in rea at reserv at elevation 12889. and E1. 2889. apacity loss annual and tot 889.0 computed d inflow for total capacit T area-capacit	0 1 38 130 266 442 663 934 1,254 S ann Creek Pro, annual runoff flow records : oir elevation 2889.0. Comp racy of the or lculated by cc The 1992 are 7.1 which was of 585 AF rec al sediment dd by ACAP usir Oct. 1991 thro y computed by ty tables for Areas in ()	2825 2830 2835 2840 2845 2855 2860 2855 2860 2865 ject, 19 value o for rese 2889.0. ited by iginal probably orded a eposits g origin bugh May ACAP us E1. 282 calcul	Reclamat surface of recompu- ured slig y due the t elevat: of 22.0 nal surface f 1992. sing 9/64 5 through ated by A	77.6 90.1 101.4 113.0 123.6 136.6 154.4 176.7 199.2 BOR. 5 AF (Ite beration Clon's AC areas. ted capa ghtly gr e differ ion 2860 AF and 5 ace area	em 24 peri CAP y acity ceate cence cence cence conconce conconce conce conce conce conce conce conce conce conce conce conce c	1,619 2,038 2,517 3,053 3,644 4,295 5,022 5,850 6,790 4). iod. (see reprised on the second se	sing mark rigin vey m tfull for El quest	2870 2875 2880 2885 2889 2890 2897.1 2903 #5) and 15 al areas (ethods and y divided 2760 thm ion as to	214.1 230.2 250.4 268.6 (283) 286.7 314.0 336.8 336.8 992 capacity at <22) at E1. 28 (/or some bank by 13,091 AF.	Some spillway 65, erosion. Capacity and areas f the

48. AGENCY MAKING SURVEY Bureau of Reclamation 49. AGENCY SUPPLYING DATA Bureau of Reclamation DATE June 1993

Table 1. - Reservoir sediment data summary (page 2 of 2).

(1) Elevation (ft)	(2) Original area (acres)	(3) Original total capacity (acre-ft)	(4) 1992 area (acres)	(5) 1992 capacity (acre-ft)	(6) Measured sediment volume (acre-ft)	(7) Measured Sediment (%)	(8) Reservoir Depth (%)
2897.1	313.0	15,502	314.0	14,955	547	100.0	100.0
2890.0	286.0	13,375	286.7	12,821	554	100.0	94.8
2889.0	283.0	13,091	283.6	12,536	555	100.0	94.1
2880.0	251.0	10,688	250.4	10,135	553	100.0	87.5
2870.0	211.0	8,383	214.1	7,823	560	100.0	80.2
2860.0	178.0	6,435	176.7	5,850	585	100.0	72.9
2850.0	144.0	4,830	136.6	4,295	535	96.4	65.6
2840.0	118.0	3,525	113.0	3,053	472	85.0	58.4
2830.0	97.0	2,448	90.1	2,038	410	73.9	51.0
2820.0	77.0	1,593	68.2	1,254	339	61.1	43.8
2810.0	56.0	930	48.8	663	267	48.1	36.5
2800.0	36.0	473	31.1	266	207	37.2	29.2
2790.0	19.0	201	13.6	38	163	29.4	21.9
2782.7	11.0	94	0.0	0	94	16.9	16.6
2780.0	8.0	. 69	0.0	0	69	12.4	14.6
2770.0	3.0	15	0.0	0	15	2.7	7.3
2760.0	0.0	0	0.0	0	0	0.0	0.0

(1) Elevation of reservoir water surface.

(2) Original reservoir surface area values.

(3) Original reservoir capacity recomputed using ACAP85.

(4) Reservoir surface area from 1992 survey.

(5) 1992 calculated reservoir capacity from 1992 survey data.

(6) Measured sediment volume = column (3) - column (5).

(7) Measured sediment expressed in percentage of total sediment (555), measured at spillway crest El. 2889. 100% measured from elevation 2860 and above. 1992 areas measured slightly greater than original at El. 2870, 2890, and 2897.1, probably due to difference in survey methods or some bank erosion.

(8) Depth of reservoir expressed in percentage of total depth (137.1 feet).

Table 2. - Summary of 1992 survey results.



Figure 1. - Mann Creek location map.

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Figure 3. - Mann Creek Reservoir topographic map.



Figure 4. - 1992 area and capacity curves.

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Mission

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The mission of the Bureau of Reclamation is to manage, develop, and protect water and related resources in an environmentally and economically sound manner in the interest of the American Public.

A free pamphlet is available from the Bureau entitled "Publications for Sale." It describes some of the technical publications currently available, their cost, and how to order them. The pamphlet can be obtained upon request from the Bureau of Reclamation, Attn D-7923H, PO Box 25007, Denver Federal Center, Denver CO 80225-0007.